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GEOTECHNICAL  
ENVIRONMENTAL  
MATERIALS

# AASHTO 2002 ASD DESIGN METHOD

## Jamestown Mall

MSEW+: Update # 2021.14

### PROJECT IDENTIFICATION

Title: Jamestown Mall  
Project Number: 15277  
Client:  
Designer: KLL  
Station Number: 0+50

### Description:

### Company's information:

Name: Midwest Testing  
Street: 8606 Page Avenue

St. Louis, MO 63114  
Telephone #: (314) 739-2727  
Fax #:  
E-Mail:

File path and name: S:\Jobs\Active Jobs\15277\RW\Engineering\MSEW\15277.Sta.....  
.....15277.Sta. 0+50.BENp

Original date and time of creating this file: Wed Sep 08 08:39:25 2021

### PROGRAM MODE:

ANALYSIS  
of a SIMPLE STRUCTURE  
using GEOGRID as reinforcing material.



**SOIL DATA**

**REINFORCED SOIL**

Unit weight, $\gamma$		130.0 lb/ft <sup>3</sup>
Design value of internal angle of friction, $\phi$		38.0°

**RETAINED SOIL**

Unit weight, $\gamma$		120.0 lb/ft <sup>3</sup>
Design value of internal angle of friction, $\phi$		26.0°

**FOUNDATION SOIL (Considered as an equivalent uniform soil)**

Equivalent unit weight, $\gamma_{equiv}$ .		120.0 lb/ft <sup>3</sup>
Equivalent internal angle of friction, $\phi_{equiv}$ .		26.0°
Equivalent cohesion, $c_{equiv}$ .		50.0 lb/ft <sup>2</sup>

Water table does not affect bearing capacity

**LATERAL EARTH PRESSURE COEFFICIENTS**

$K_a$  (internal stability) = 0.2379 (if batter is less than 10°,  $K_a$  is calculated from eq. 15. Otherwise, eq. 38 is utilized)  
 Inclination of internal slip plane,  $\psi = 64.00^\circ$  (see Fig. 28 in DEMO 82).  
 $K_a$  (external stability) = 0.4787 (eq. 17 is utilized to calculate  $K_a$  for all batters)  
 ( For external stability user specified  $\delta = 0.00^\circ$  )

**BEARING CAPACITY**

Bearing capacity is controlled by general shear.  
 Bearing capacity factors (calculated by MSEW):  $N_c = 22.25$      $N \gamma = 12.54$

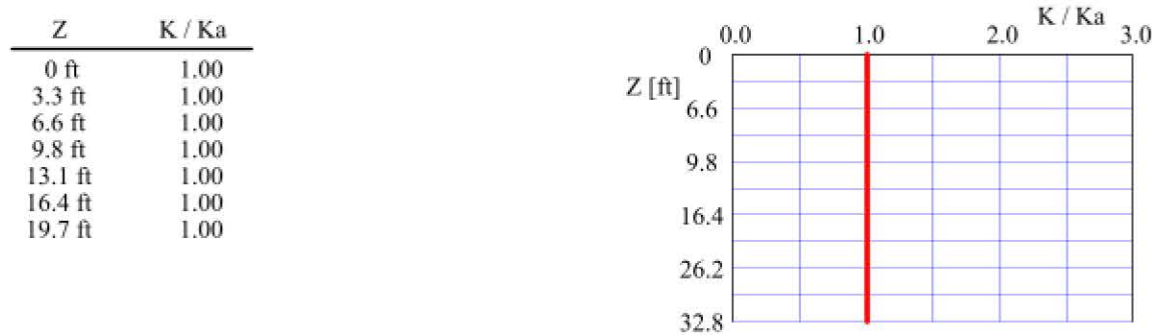
**SEISMICITY**

Not Applicable

**INPUT DATA: Geogrids  
(Analysis)**

D A T A	Geogrid type #1	Geogrid type #2	Geogrid type #3	Geogrid type #4	Geogrid type #5
Tult [lb/ft]	3437.0	4815.0	8025.0		
Durability reduction factor, RFd	1.10	1.10	1.10		
Installation-damage reduction factor, RFid	1.05	1.05	1.05		
Creep reduction factor, RFc	1.55	1.55	1.55	N/A	N/A
Fs-overall for strength	N/A	N/A	N/A		
Coverage ratio, Rc	1.000	1.000	1.000		
Friction angle along geogrid-soil interface, $\rho$	27.52	27.52	27.52		
Pullout resistance factor, $F^*$	$0.67 \cdot \tan \phi$	$0.67 \cdot \tan \phi$	$0.67 \cdot \tan \phi$	N/A	N/A
Scale-effect correction factor, $\alpha$	0.8	0.8	0.8		

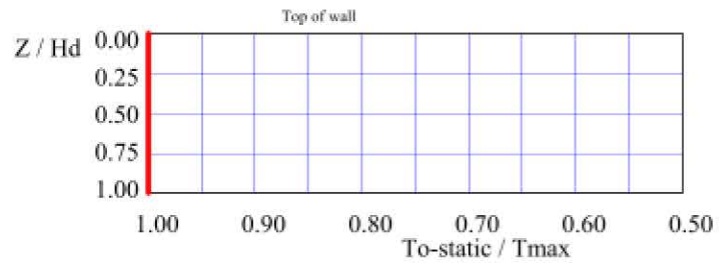
**Variation of Lateral Earth Pressure Coefficient With Depth**



**INPUT DATA: Facia and Connection (according to revised Demo 82)  
(Analysis)**

FACIA type: Facing enabling frictional connection of reinforcement (e.g., modular concrete blocks, gabions)  
 Depth/height of block is 1.00/0.67 ft. Horizontal distance to Center of Gravity of block is: 0.50 ft.  
 Average unit weight of block is:  $\gamma_r = 120.00 \text{ lb/ft}^3$

Z / Hd	To-static / Tmax
0.00	1.00
0.25	1.00
0.50	1.00
0.75	1.00
1.00	1.00



Geogrid Type #1		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma^{(1)}$	CRult <sup>(2)</sup>	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult
0.0	0.40	0.0	0.33	0.0	0.29				
2000.0	0.43	2000.0	0.49	2000.0	0.39	N/A		N/A	

Geogrid Type #1 <sup>(3)</sup>		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr
0.0	0.31	0.0	0.25	0.0	0.17				
2000.0	0.35	2000.0	0.39	2000.0	0.27	N/A		N/A	

<sup>(1)</sup>  $\sigma$  = Confining stress in between stacked blocks [lb/ft<sup>2</sup>]  
<sup>(2)</sup> CRult = Tc-ult / Tult  
<sup>(3)</sup> CRcr = Tere / Tult

D A T A (for connection only)	Type #1	Type #2	Type #3	Type #4	Type #5
Product Name	HP200	HP300	HP500	N/A	N/A
Connection strength reduction factor, RFd	1.00	1.00	1.00	N/A	N/A
Creep reduction factor, RFC	N/A	N/A	N/A	N/A	N/A

**INPUT DATA: Geometry and Surcharge loads (of a SIMPLE STRUCTURE)**

Design height,  $H_d$       7.67 [ft]      { Embedded depth is  $E = 0.67$  ft, and height above top of finished bottom grade is  $H = 7.00$  ft }

Soil in front of wall is Horizontal.

Batter,  $\omega$                 0.0 [deg]

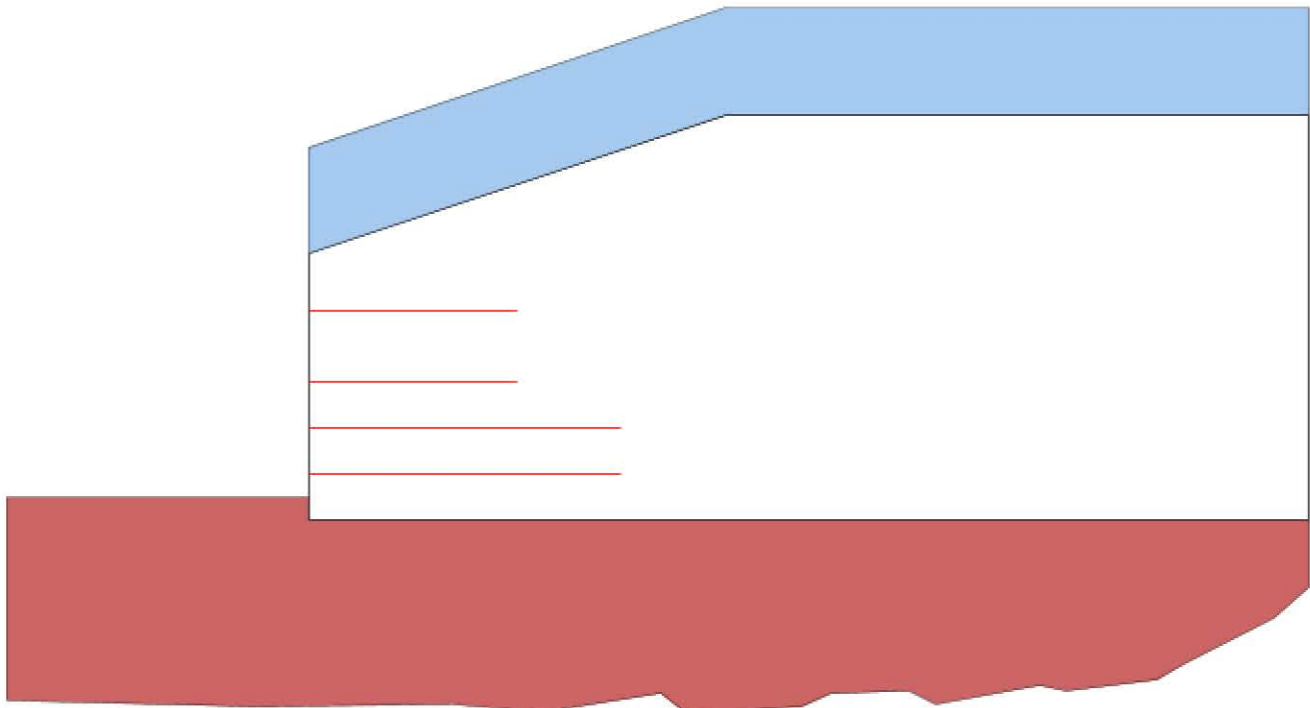
Backslope,  $\beta$             18.4 [deg]

Backslope rise            4.0 [ft]                Broken back equivalent angle,  $I = 14.61^\circ$  (see Fig. 25 in DEMO 82)

**UNIFORM SURCHARGE**

Uniformly distributed dead load is 0.0 [lb/ft<sup>2</sup>], and live load is 100.0 [lb/ft<sup>2</sup>]

**ANALYZED REINFORCEMENT LAYOUT:**



**SCALE:**









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GEOTECHNICAL  
ENVIRONMENTAL  
MATERIALS

# AASHTO 2002 ASD DESIGN METHOD

## Jamestown Mall

MSEW+: Update # 2021.14

### PROJECT IDENTIFICATION

Title: Jamestown Mall  
Project Number: 15277  
Client:  
Designer: KLL  
Station Number: 0+75

### Description:

### Company's information:

Name: Midwest Testing  
Street: 8606 Page Avenue

St. Louis, MO 63114  
Telephone #: (314) 739-2727  
Fax #:  
E-Mail:

File path and name: S:\Jobs\Active Jobs\15277\RW\Engineering\MSEW\15277.Sta.....  
.....15277.Sta. 0+75.BENp

Original date and time of creating this file: Wed Sep 08 08:39:25 2021

### PROGRAM MODE:

ANALYSIS  
of a SIMPLE STRUCTURE  
using GEOGRID as reinforcing material.

**SOIL DATA****REINFORCED SOIL**

Unit weight,  $\gamma$  130.0 lb/ft<sup>3</sup>  
 Design value of internal angle of friction,  $\phi$  38.0 °

**RETAINED SOIL**

Unit weight,  $\gamma$  120.0 lb/ft<sup>3</sup>  
 Design value of internal angle of friction,  $\phi$  26.0 °

**FOUNDATION SOIL (Considered as an equivalent uniform soil)**

Equivalent unit weight,  $\gamma_{equiv.}$  120.0 lb/ft<sup>3</sup>  
 Equivalent internal angle of friction,  $\phi_{equiv.}$  26.0 °  
 Equivalent cohesion,  $c_{equiv.}$  50.0 lb/ft<sup>2</sup>

Water table does not affect bearing capacity

**LATERAL EARTH PRESSURE COEFFICIENTS**

$K_a$  (internal stability) = 0.2379 (if batter is less than 10°,  $K_a$  is calculated from eq. 15. Otherwise, eq. 38 is utilized)

Inclination of internal slip plane,  $\psi = 64.00^\circ$  (see Fig. 28 in DEMO 82).

$K_a$  (external stability) = 0.5744 (eq. 17 is utilized to calculate  $K_a$  for all batters)

( For external stability user specified  $\delta = 0.00^\circ$  )

**BEARING CAPACITY**

Bearing capacity is controlled by general shear.

Bearing capacity factors (calculated by MSEW):  $N_c = 22.25$

$N \gamma = 12.54$

**SEISMICITY**

Not Applicable

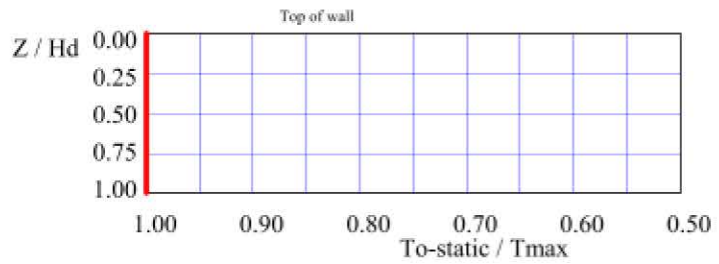




**INPUT DATA: Facia and Connection (according to revised Demo 82)  
(Analysis)**

FACIA type: Facing enabling frictional connection of reinforcement (e.g., modular concrete blocks, gabions)  
 Depth/height of block is 1.00/0.67 ft. Horizontal distance to Center of Gravity of block is: 0.50 ft.  
 Average unit weight of block is:  $\gamma_r = 120.00 \text{ lb/ft}^3$

Z / Hd	To-static / Tmax
0.00	1.00
0.25	1.00
0.50	1.00
0.75	1.00
1.00	1.00



Geogrid Type #1		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma^{(1)}$	CRult <sup>(2)</sup>	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult
0.0	0.40	0.0	0.33	0.0	0.29				
2000.0	0.43	2000.0	0.49	2000.0	0.39	N/A		N/A	

Geogrid Type #1 <sup>(3)</sup>		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr
0.0	0.31	0.0	0.25	0.0	0.17				
2000.0	0.35	2000.0	0.39	2000.0	0.27	N/A		N/A	

<sup>(1)</sup>  $\sigma$  = Confining stress in between stacked blocks [lb/ft<sup>2</sup>]  
<sup>(2)</sup> CRult = Tc-ult / Tult  
<sup>(3)</sup> CRcr = Tere / Tult

D A T A (for connection only)	Type #1	Type #2	Type #3	Type #4	Type #5
Product Name	HP200	HP300	HP500	N/A	N/A
Connection strength reduction factor, RFd	1.00	1.00	1.00	N/A	N/A
Creep reduction factor, RFc	N/A	N/A	N/A	N/A	N/A

**INPUT DATA: Geometry and Surcharge loads (of a SIMPLE STRUCTURE)**

Design height, Hd      7.34 [ft]      { Embedded depth is E = 0.67 ft, and height above top of finished bottom grade is H = 6.67 ft }

Soil in front of wall is Horizontal.

Batter,  $\omega$               0.0 [deg]

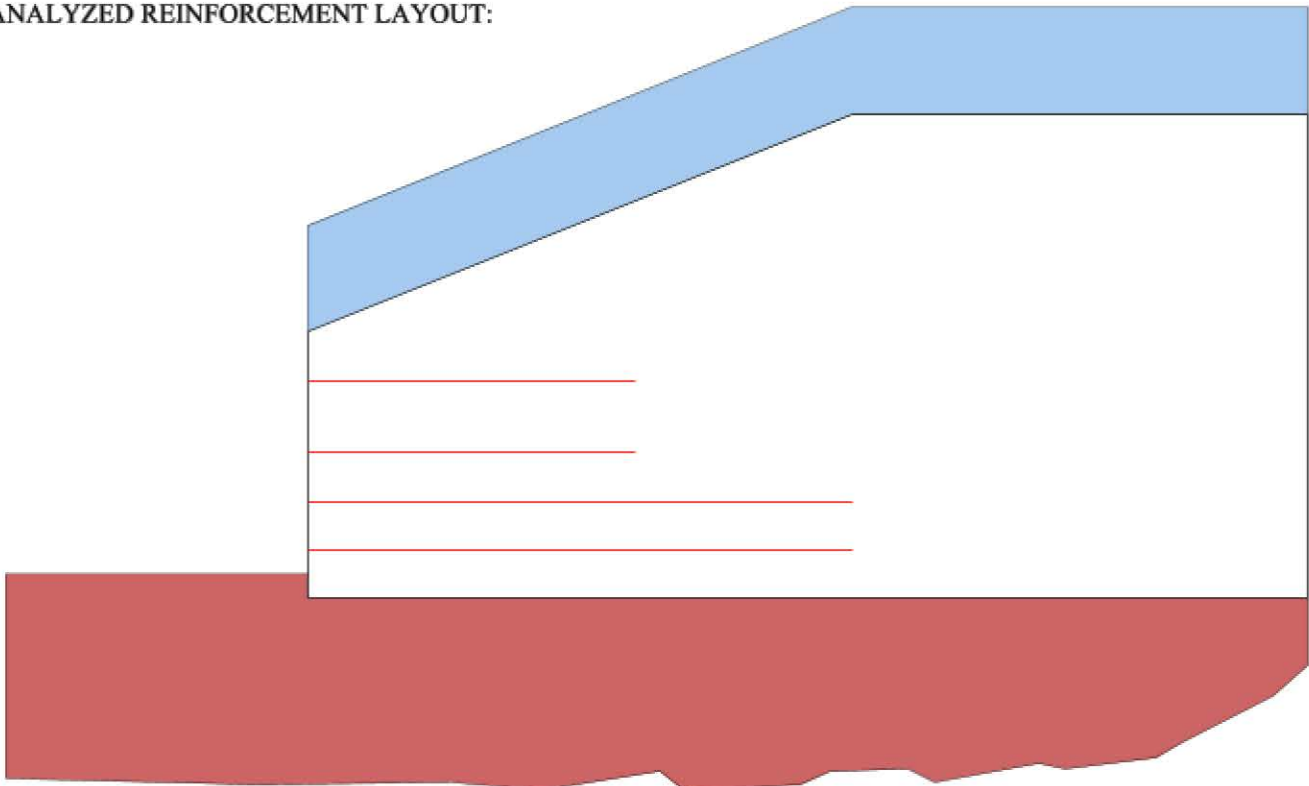
Backslope,  $\beta$          21.8 [deg]

Backslope rise         6.0 [ft]              Broken back equivalent angle, I = 21.80° (see Fig. 25 in DEMO 82)

**UNIFORM SURCHARGE**

Uniformly distributed dead load is 0.0 [lb/ft<sup>2</sup>], and live load is 100.0 [lb/ft<sup>2</sup>]

**ANALYZED REINFORCEMENT LAYOUT:**



**SCALE:**







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# AASHTO 2002 ASD DESIGN METHOD

## Jamestown Mall

MSEW+: Update # 2021.14

### PROJECT IDENTIFICATION

Title: Jamestown Mall  
Project Number: 15277  
Client:  
Designer: KLL  
Station Number: 1+25

### Description:

### Company's information:

Name: Midwest Testing  
Street: 8606 Page Avenue

St. Louis, MO 63114  
Telephone #: (314) 739-2727  
Fax #:  
E-Mail:

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.....15277.Sta. 1+25.BENp

Original date and time of creating this file: Wed Sep 08 08:39:25 2021

### PROGRAM MODE:

ANALYSIS  
of a SIMPLE STRUCTURE  
using GEOGRID as reinforcing material.

### SOIL DATA

#### REINFORCED SOIL

Unit weight, $\gamma$		130.0 lb/ft <sup>3</sup>
Design value of internal angle of friction, $\phi$		38.0 °

#### RETAINED SOIL

Unit weight, $\gamma$		120.0 lb/ft <sup>3</sup>
Design value of internal angle of friction, $\phi$		26.0 °

#### FOUNDATION SOIL (Considered as an equivalent uniform soil)

Equivalent unit weight, $\gamma_{equiv.}$		120.0 lb/ft <sup>3</sup>
Equivalent internal angle of friction, $\phi_{equiv.}$		26.0 °
Equivalent cohesion, $c_{equiv.}$		50.0 lb/ft <sup>2</sup>

Water table does not affect bearing capacity

### LATERAL EARTH PRESSURE COEFFICIENTS

$K_a$  (internal stability) = 0.2379 (if batter is less than 10°,  $K_a$  is calculated from eq. 15. Otherwise, eq. 38 is utilized)  
 Inclination of internal slip plane,  $\psi = 64.00^\circ$  (see Fig. 28 in DEMO 82).  
 $K_a$  (external stability) = 0.5744 (eq. 17 is utilized to calculate  $K_a$  for all batters)  
 ( For external stability user specified  $\delta = 0.00^\circ$  )

### BEARING CAPACITY

Bearing capacity is controlled by general shear.  
 Bearing capacity factors (calculated by MSEW):  $N_c = 22.25$                        $N \gamma = 12.54$

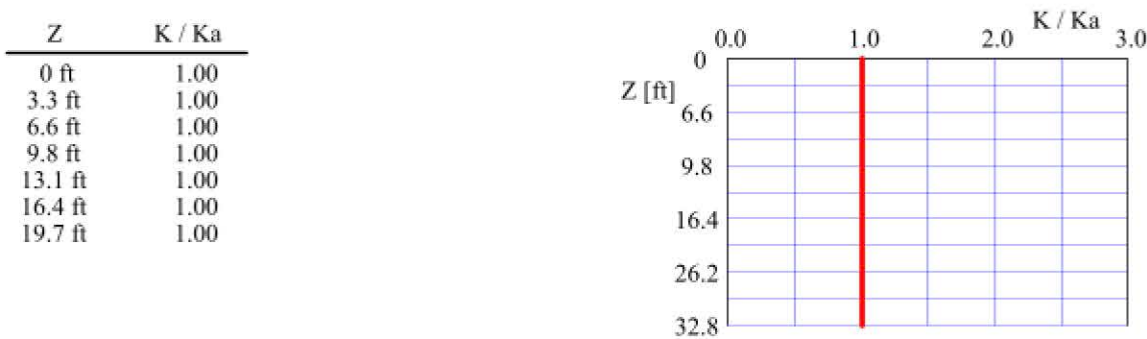
### SEISMICITY

Not Applicable

**INPUT DATA: Geogrids  
(Analysis)**

D A T A	Geogrid type #1	Geogrid type #2	Geogrid type #3	Geogrid type #4	Geogrid type #5
Tult [lb/ft]	3437.0	4815.0	8025.0		
Durability reduction factor, RFD	1.10	1.10	1.10		
Installation-damage reduction factor, RFid	1.05	1.05	1.05		
Creep reduction factor, RFc	1.55	1.55	1.55	N/A	N/A
Fs-overall for strength	N/A	N/A	N/A		
Coverage ratio, Rc	1.000	1.000	1.000		
Friction angle along geogrid-soil interface, $\rho$	27.52	27.52	27.52		
Pullout resistance factor, F*	$0.67 \cdot \tan \phi$	$0.67 \cdot \tan \phi$	$0.67 \cdot \tan \phi$	N/A	N/A
Scale-effect correction factor, $\alpha$	0.8	0.8	0.8		

**Variation of Lateral Earth Pressure Coefficient With Depth**

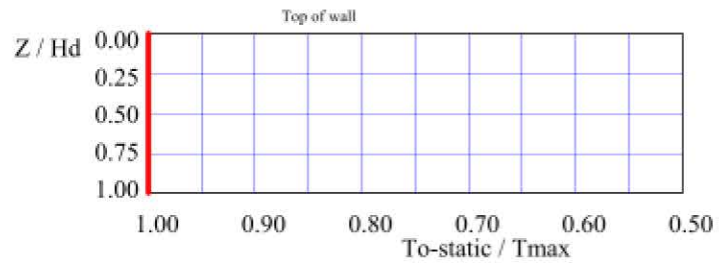




**INPUT DATA: Facia and Connection (according to revised Demo 82)  
(Analysis)**

FACIA type: Facing enabling frictional connection of reinforcement (e.g., modular concrete blocks, gabions)  
 Depth/height of block is 1.00/0.67 ft. Horizontal distance to Center of Gravity of block is: 0.50 ft.  
 Average unit weight of block is:  $\gamma_r = 120.00 \text{ lb/ft}^3$

Z / Hd	To-static / Tmax
0.00	1.00
0.25	1.00
0.50	1.00
0.75	1.00
1.00	1.00



Geogrid Type #1		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma^{(1)}$	CRult <sup>(2)</sup>	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult
0.0	0.40	0.0	0.33	0.0	0.29				
2000.0	0.43	2000.0	0.49	2000.0	0.39	N/A		N/A	

Geogrid Type #1 <sup>(3)</sup>		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr
0.0	0.31	0.0	0.25	0.0	0.17				
2000.0	0.35	2000.0	0.39	2000.0	0.27	N/A		N/A	

<sup>(1)</sup>  $\sigma$  = Confining stress in between stacked blocks [lb/ft<sup>2</sup>]  
<sup>(2)</sup> CRult = Tc-ult / Tult  
<sup>(3)</sup> CRcr = Tere / Tult

D A T A (for connection only)	Type #1	Type #2	Type #3	Type #4	Type #5
Product Name	HP200	HP300	HP500	N/A	N/A
Connection strength reduction factor, RFd	1.00	1.00	1.00	N/A	N/A
Creep reduction factor, RFc	N/A	N/A	N/A	N/A	N/A

**INPUT DATA: Geometry and Surcharge loads (of a SIMPLE STRUCTURE)**

Design height, Hd      6.34 [ft]      { Embedded depth is E = 0.67 ft, and height above top of finished bottom grade is H = 5.67 ft }

Soil in front of wall is Horizontal.

Batter,  $\omega$               0.0 [deg]

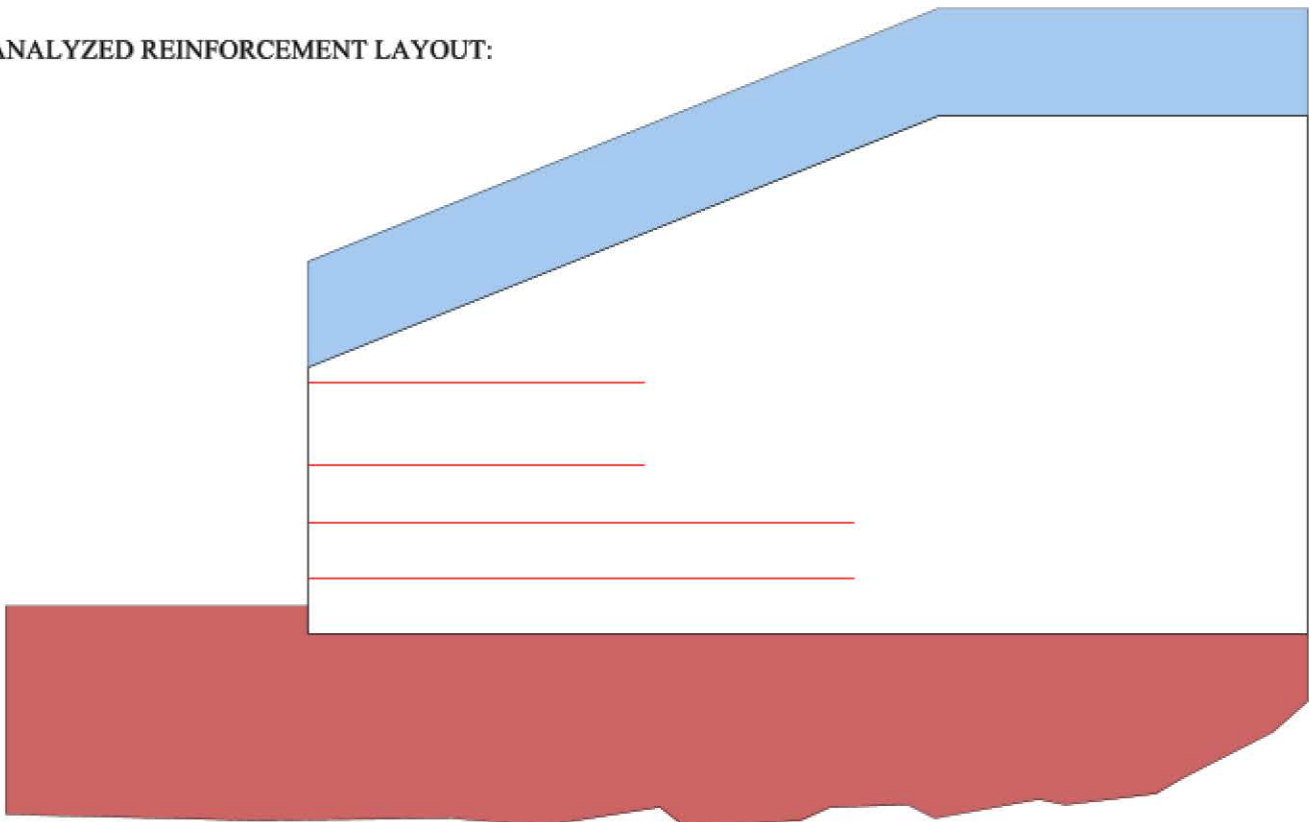
Backslope,  $\beta$          21.8 [deg]

Backslope rise         6.0 [ft]              Broken back equivalent angle, I = 21.80° (see Fig. 25 in DEMO 82)

**UNIFORM SURCHARGE**

Uniformly distributed dead load is 0.0 [lb/ft<sup>2</sup>], and live load is 100.0 [lb/ft<sup>2</sup>]

**ANALYZED REINFORCEMENT LAYOUT:**



**SCALE:**



**ANALYSIS: CALCULATED FACTORS (Static conditions)**

Bearing capacity,  $F_s = 6.89$ , Meyerhof stress = 1422 lb/ft<sup>2</sup>.

Foundation Interface: Direct sliding,  $F_s = 1.527$ , Eccentricity,  $e/L = 0.0609$ ,  $F_s$ -overturning = 5.02

#	GEOGRID			CONNECTION		Geogrid strength $F_s$	Pullout resistance $F_s$	Direct sliding $F_s$	Eccentricity $e/L$	Product name
	Elevation [ft]	Length [ft]	Type #	$F_s$ -overall [connection strength]	$F_s$ -overall [geogrid strength]					
1	1.33	13.00	1	2.56	4.44	4.436	23.943	1.604	0.0341	HP200
2	2.67	13.00	1	4.98	8.73	8.726	37.632	1.715	0.0055	HP200
3	4.00	8.00	1	5.50	9.74	9.737	14.398	1.552	0.0188	HP200
4	6.00	8.00	1	11.08	19.91	19.911	14.396	1.655	-0.0836	HP200



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MATERIALS

# AASHTO 2002 ASD DESIGN METHOD

## Jamestown Mall

MSEW+: Update # 2021.14

### PROJECT IDENTIFICATION

Title: Jamestown Mall  
Project Number: 15277  
Client:  
Designer: KLL  
Station Number: 1+82

### Description:

### Company's information:

Name: Midwest Testing  
Street: 8606 Page Avenue

St. Louis, MO 63114  
Telephone #: (314) 739-2727  
Fax #:  
E-Mail:

File path and name: S:\Jobs\Active Jobs\15277\RW\Engineering\MSEW\15277.Sta.....  
.....15277.Sta. 1+82.BENp

Original date and time of creating this file: Wed Sep 08 08:39:25 2021

### PROGRAM MODE:

ANALYSIS  
of a SIMPLE STRUCTURE  
using GEOGRID as reinforcing material.

**SOIL DATA****REINFORCED SOIL**

Unit weight,  $\gamma$  130.0 lb/ft<sup>3</sup>  
 Design value of internal angle of friction,  $\phi$  38.0 °

**RETAINED SOIL**

Unit weight,  $\gamma$  120.0 lb/ft<sup>3</sup>  
 Design value of internal angle of friction,  $\phi$  26.0 °

**FOUNDATION SOIL (Considered as an equivalent uniform soil)**

Equivalent unit weight,  $\gamma_{equiv.}$  120.0 lb/ft<sup>3</sup>  
 Equivalent internal angle of friction,  $\phi_{equiv.}$  26.0 °  
 Equivalent cohesion,  $c_{equiv.}$  50.0 lb/ft<sup>2</sup>

Water table does not affect bearing capacity

**LATERAL EARTH PRESSURE COEFFICIENTS**

$K_a$  (internal stability) = 0.2379 (if batter is less than 10°,  $K_a$  is calculated from eq. 15. Otherwise, eq. 38 is utilized)

Inclination of internal slip plane,  $\psi = 64.00^\circ$  (see Fig. 28 in DEMO 82).

$K_a$  (external stability) = 0.5744 (eq. 17 is utilized to calculate  $K_a$  for all batters)

( For external stability user specified  $\delta = 0.00^\circ$  )

**BEARING CAPACITY**

Bearing capacity is controlled by general shear.

Bearing capacity factors (calculated by MSEW):  $N_c = 22.25$

$N \gamma = 12.54$

**SEISMICITY**

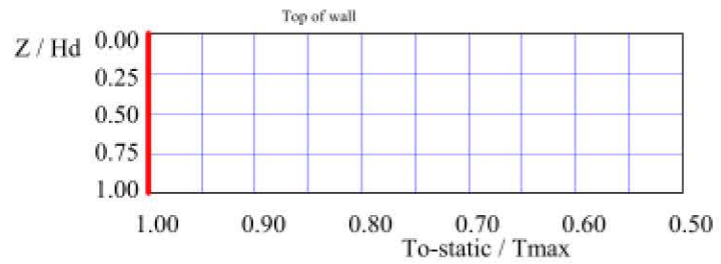
Not Applicable



**INPUT DATA: Facia and Connection (according to revised Demo 82)  
(Analysis)**

FACIA type: Facing enabling frictional connection of reinforcement (e.g., modular concrete blocks, gabions)  
 Depth/height of block is 1.00/0.67 ft. Horizontal distance to Center of Gravity of block is: 0.50 ft.  
 Average unit weight of block is:  $\gamma_r = 120.00 \text{ lb/ft}^3$

Z / Hd	To-static / Tmax
0.00	1.00
0.25	1.00
0.50	1.00
0.75	1.00
1.00	1.00



Geogrid Type #1		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma^{(1)}$	CRult <sup>(2)</sup>	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult
0.0	0.40	0.0	0.33	0.0	0.29				
2000.0	0.43	2000.0	0.49	2000.0	0.39	N/A		N/A	

Geogrid Type #1 <sup>(3)</sup>		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr
0.0	0.31	0.0	0.25	0.0	0.17				
2000.0	0.35	2000.0	0.39	2000.0	0.27	N/A		N/A	

<sup>(1)</sup>  $\sigma$  = Confining stress in between stacked blocks [lb/ft<sup>2</sup>]  
<sup>(2)</sup> CRult = Tc-ult / Tult  
<sup>(3)</sup> CRcr = Tere / Tult

D A T A (for connection only)	Type #1	Type #2	Type #3	Type #4	Type #5
Product Name	HP200	HP300	HP500	N/A	N/A
Connection strength reduction factor, RFd	1.00	1.00	1.00	N/A	N/A
Creep reduction factor, RFc	N/A	N/A	N/A	N/A	N/A



**INPUT DATA: Geometry and Surcharge loads (of a SIMPLE STRUCTURE)**

Design height, Hd 4.34 [ft] { Embedded depth is E = 0.67 ft, and height above top of finished bottom grade is H = 3.67 ft }

Soil in front of wall is Horizontal.

Batter,  $\omega$  0.0 [deg]

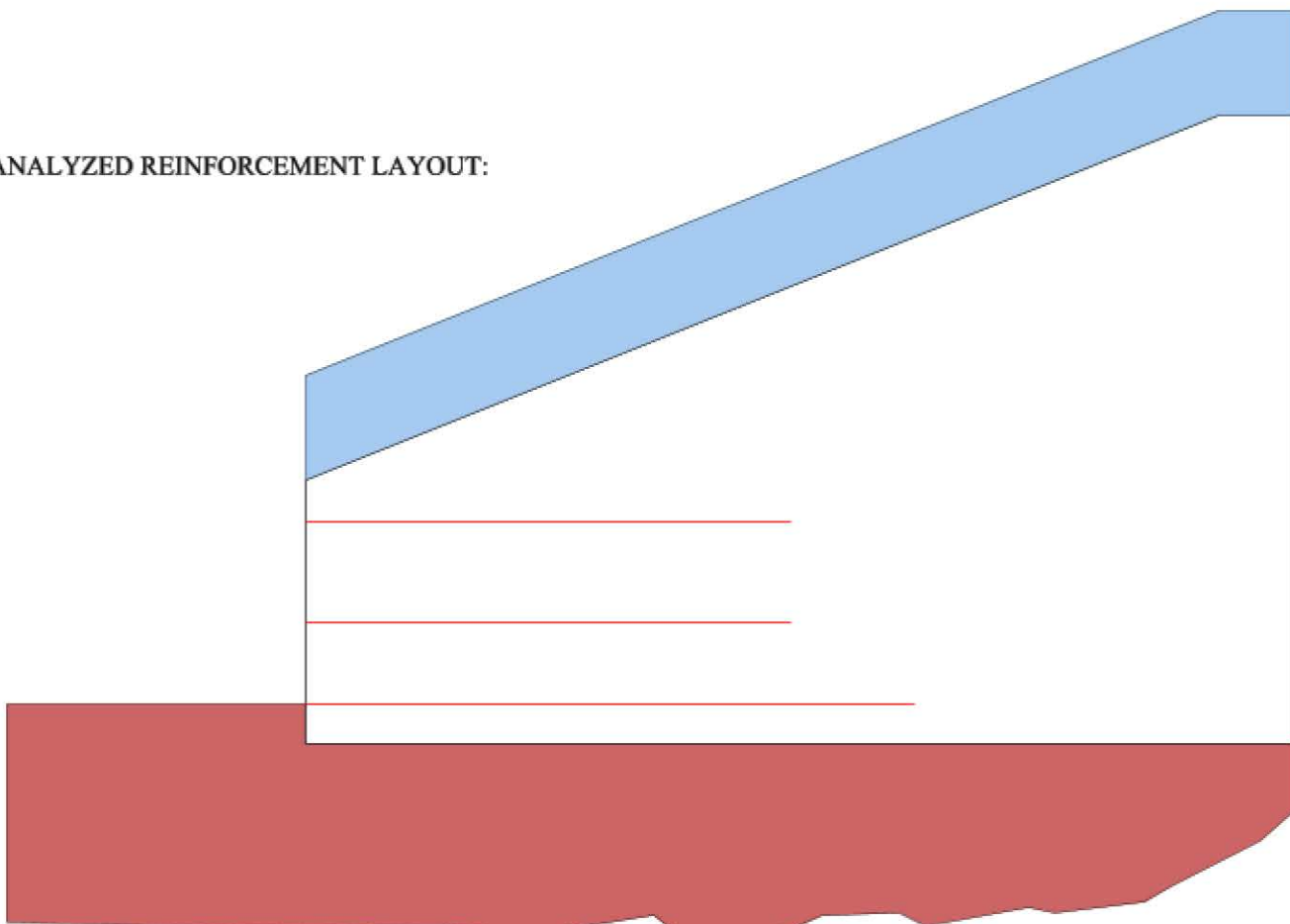
Backslope,  $\beta$  21.8 [deg]

Backslope rise 6.0 [ft] Broken back equivalent angle, I = 21.80° (see Fig. 25 in DEMO 82)

**UNIFORM SURCHARGE**

Uniformly distributed dead load is 0.0 [lb/ft<sup>2</sup>], and live load is 100.0 [lb/ft<sup>2</sup>]

**ANALYZED REINFORCEMENT LAYOUT:**



**SCALE:**



ANALYSIS: CALCULATED FACTORS (Static conditions)

Bearing capacity,  $F_s = 7.78$ , Meyerhof stress = 1020 lb/ft<sup>2</sup>.

Foundation Interface: Direct sliding,  $F_s = 1.572$ , Eccentricity,  $e/L = 0.0525$ ,  $F_s$ -overturning = 5.26

#	GEOGRID			CONNECTION		Geogrid strength $F_s$	Pullout resistance $F_s$	Direct sliding $F_s$	Eccentricity $e/L$	Product name
	Elevation [ft]	Length [ft]	Type #	$F_s$ -overall [connection strength]	$F_s$ -overall [geogrid strength]					
1	0.67	10.00	1	5.26	9.21	9.210	28.845	1.557	0.0344	HP200
2	2.00	8.00	1	6.44	11.40	11.396	18.686	1.552	0.0188	HP200
3	3.67	8.00	1	10.81	19.37	19.373	17.844	1.666	-0.0595	HP200



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GEOTECHNICAL  
ENVIRONMENTAL  
MATERIALS

# AASHTO 2002 ASD DESIGN METHOD

## Jamestown Mall

MSEW+: Update # 2021.14

### PROJECT IDENTIFICATION

Title: Jamestown Mall  
Project Number: 15277  
Client:  
Designer: KLL  
Station Number: 2+00

### Description:

### Company's information:

Name: Midwest Testing  
Street: 8606 Page Avenue

St. Louis, MO 63114  
Telephone #: (314) 739-2727  
Fax #:  
E-Mail:

File path and name: S:\Jobs\Active Jobs\15277\RW\Engineering\MSEW\15277.Sta.....  
.....15277.Sta. 2+00.BENp

Original date and time of creating this file: Wed Sep 08 08:39:25 2021

### PROGRAM MODE:

ANALYSIS  
of a SIMPLE STRUCTURE  
using GEOGRID as reinforcing material.

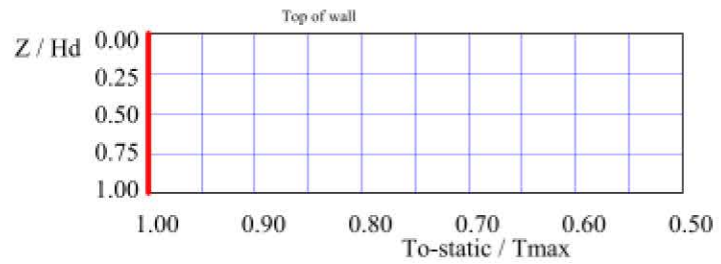




**INPUT DATA: Facia and Connection (according to revised Demo 82)  
(Analysis)**

FACIA type: Facing enabling frictional connection of reinforcement (e.g., modular concrete blocks, gabions)  
 Depth/height of block is 1.00/0.67 ft. Horizontal distance to Center of Gravity of block is: 0.50 ft.  
 Average unit weight of block is:  $\gamma_r = 120.00 \text{ lb/ft}^3$

Z / Hd	To-static / Tmax
0.00	1.00
0.25	1.00
0.50	1.00
0.75	1.00
1.00	1.00



Geogrid Type #1		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma^{(1)}$	CRult <sup>(2)</sup>	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult	$\sigma$	CRult
0.0	0.40	0.0	0.33	0.0	0.29				
2000.0	0.43	2000.0	0.49	2000.0	0.39	N/A		N/A	

Geogrid Type #1 <sup>(3)</sup>		Geogrid Type #2		Geogrid Type #3		Geogrid Type #4		Geogrid Type #5	
$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr	$\sigma$	CRcr
0.0	0.31	0.0	0.25	0.0	0.17				
2000.0	0.35	2000.0	0.39	2000.0	0.27	N/A		N/A	

<sup>(1)</sup>  $\sigma$  = Confining stress in between stacked blocks [lb/ft<sup>2</sup>]  
<sup>(2)</sup> CRult = Tc-ult / Tult  
<sup>(3)</sup> CRcr = Tere / Tult

D A T A (for connection only)	Type #1	Type #2	Type #3	Type #4	Type #5
Product Name	HP200	HP300	HP500	N/A	N/A
Connection strength reduction factor, RFd	1.00	1.00	1.00	N/A	N/A
Creep reduction factor, RFc	N/A	N/A	N/A	N/A	N/A

**INPUT DATA: Geometry and Surcharge loads (of a SIMPLE STRUCTURE)**

Design height, Hd      4.34 [ft]      { Embedded depth is E = 0.67 ft, and height above top of finished bottom grade is H = 3.67 ft }

Soil in front of wall is Horizontal.

Batter,  $\omega$               0.0 [deg]

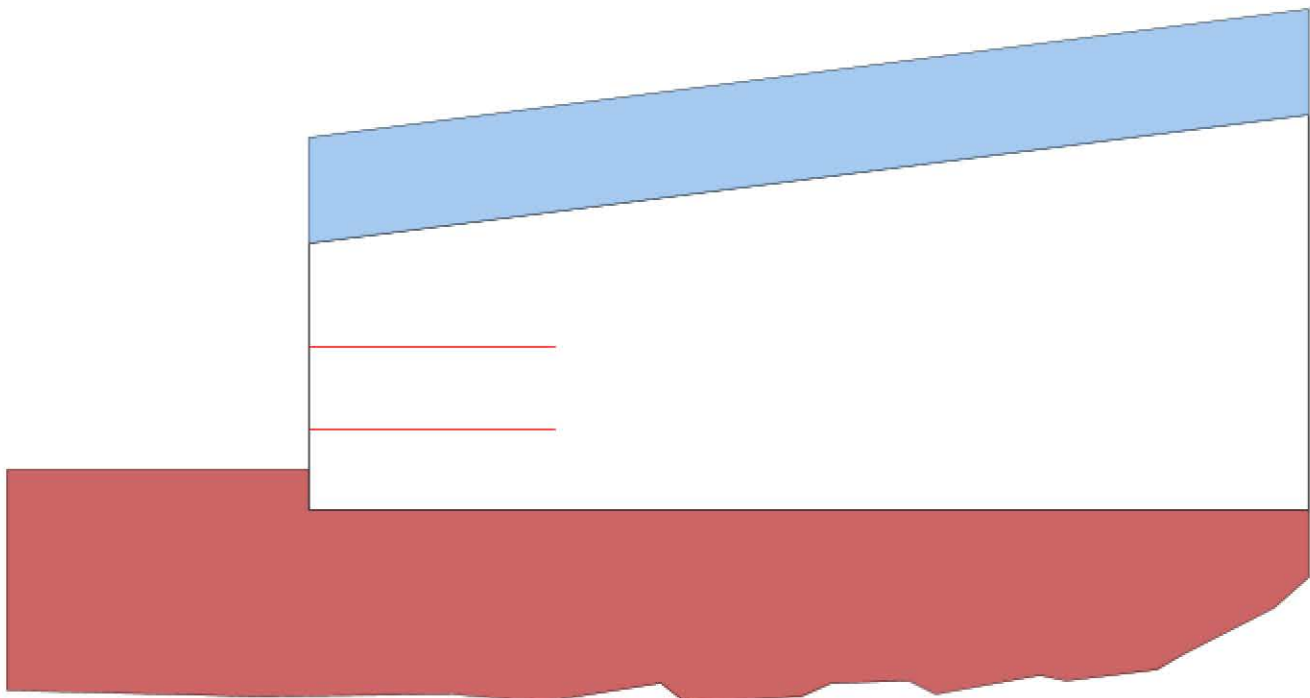
Backslope,  $\beta$          7.3 [deg]

Backslope rise         5.0 [ft]              Broken back equivalent angle, I = 7.30° (see Fig. 25 in DEMO 82)

**UNIFORM SURCHARGE**

Uniformly distributed dead load is 0.0 [lb/ft<sup>2</sup>], and live load is 100.0 [lb/ft<sup>2</sup>]

**ANALYZED REINFORCEMENT LAYOUT:**



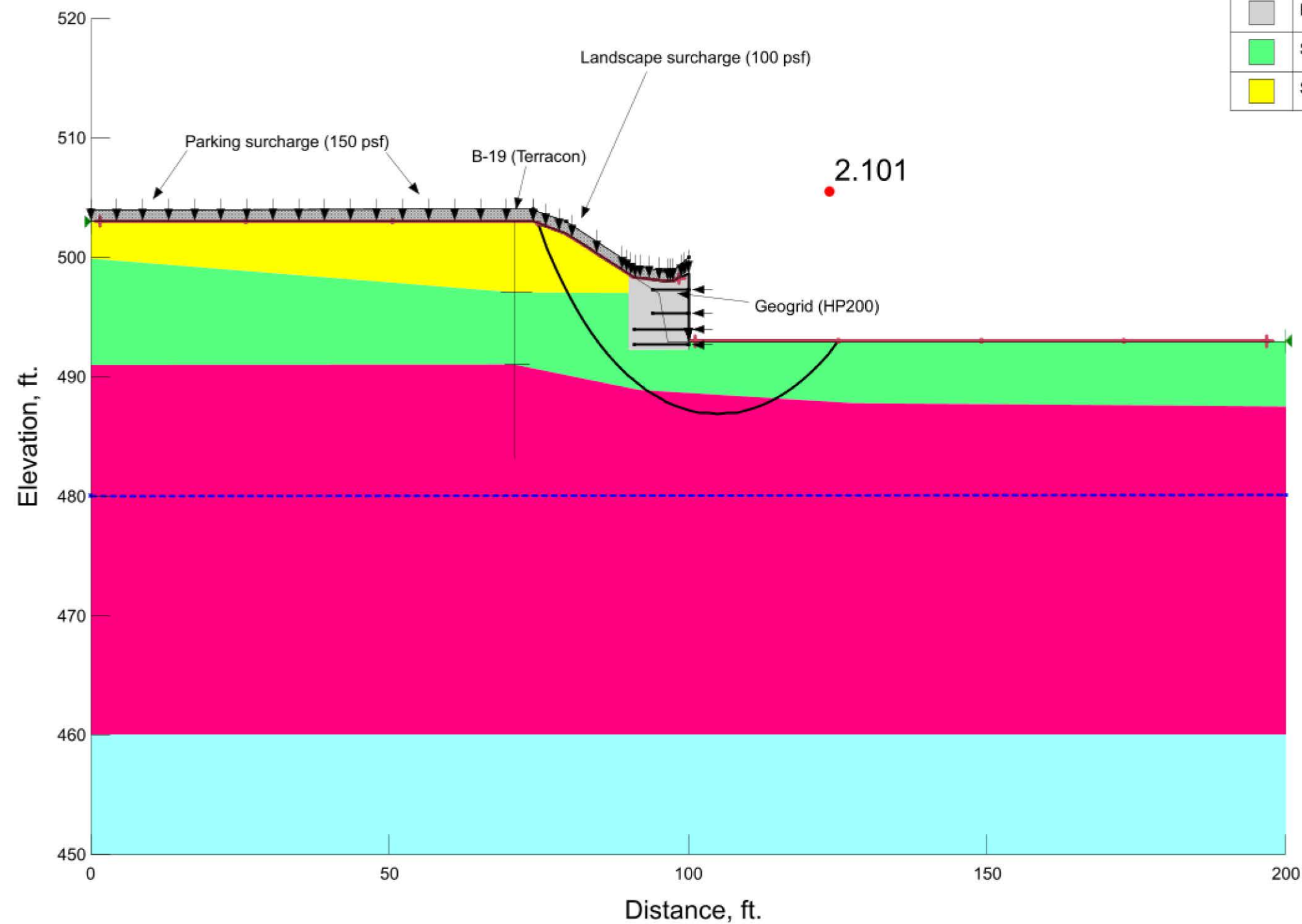
**SCALE:**





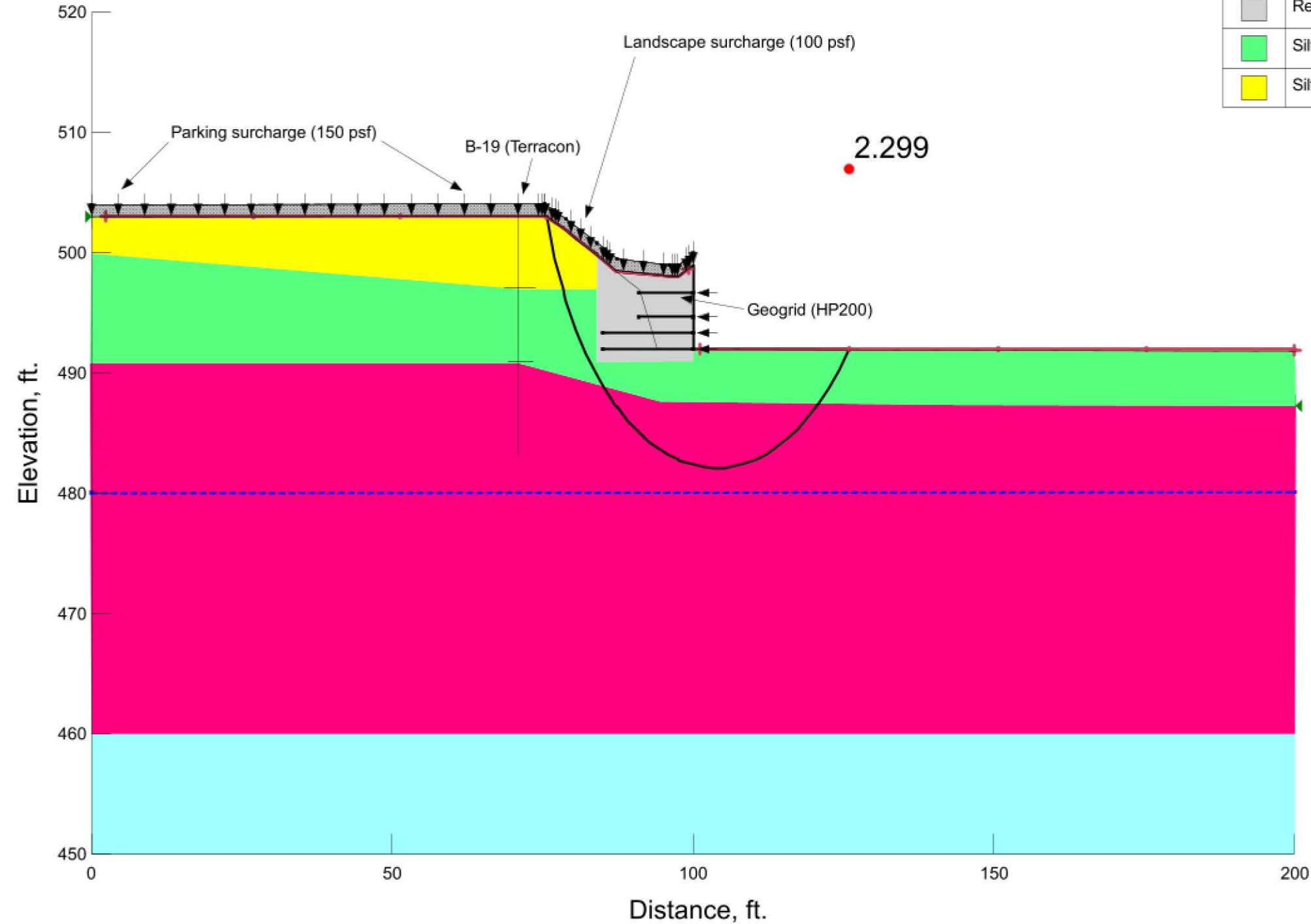


Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
Red	Clay (CH)	Mohr-Coulomb	115	0	22
Cyan	Limestone	Bedrock (Impenetrable)			
Grey	Reinforced	Mohr-Coulomb	130	0	38
Green	Silty Clay (CL)	Mohr-Coulomb	120	0	26
Yellow	Silty Clay Fill	Mohr-Coulomb	120	0	26

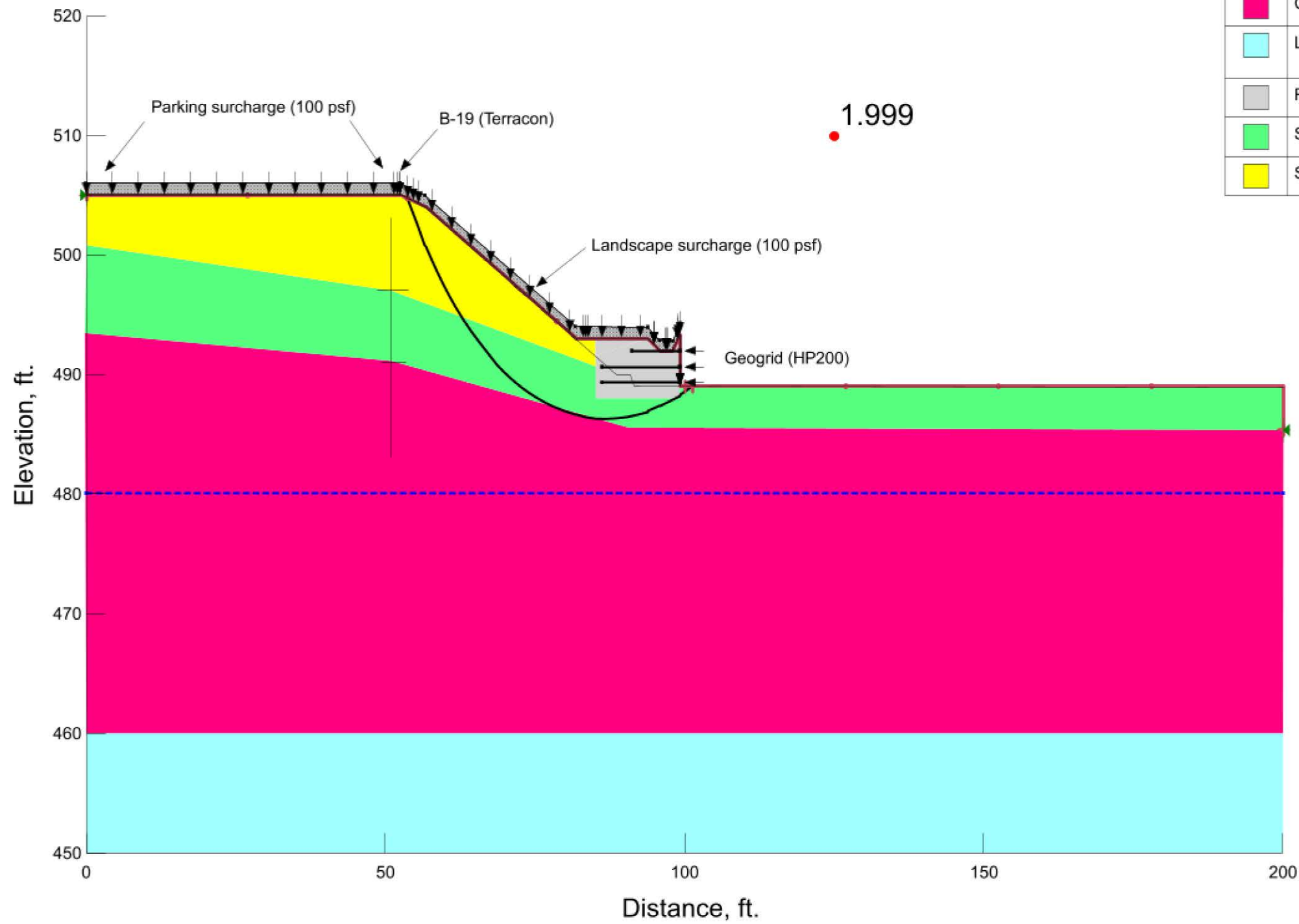


Global Stability  
 Jamestown Mall  
 Retaining Wall  
 Sta. 0+50 (3:1 Slope)

Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
Red	Clay (CH)	Mohr-Coulomb	115	0	22
Cyan	Limestone	Bedrock (Impenetrable)			
Grey	Reinforced	Mohr-Coulomb	130	0	38
Green	Silty Clay (CL)	Mohr-Coulomb	120	0	26
Yellow	Silty Clay Fill	Mohr-Coulomb	120	0	26



Global Stability  
 Jamestown Mall  
 Retaining Wall  
 Sta. 0+75 (2.5:1 Slope)



Color	Name	Model	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
■	Clay (CH)	Mohr-Coulomb	115	0	22
■	Limestone	Bedrock (Impenetrable)			
■	Reinforced	Mohr-Coulomb	130	0	38
■	Silty Clay (CL)	Mohr-Coulomb	120	0	26
■	Silty Clay Fill	Mohr-Coulomb	120	0	26

Global Stability  
 Jamestown Mall  
 Retaining Wall  
 Sta. 1+60 (2:1 Slope)